

METHOD FOR DETERMINATION OF THE DISTANCE BETWEEN ELECTRODES TO ELECTROHYDRAULIC UNDERWATER THROUGH SCINTILLAS DISCHARGE

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Abstract: In this paper to present a method for fast-track determination of the distance between electrodes to the discharge of the energy from a condensator batherry for a realize electrohydraulic effect, in function of the principal work parameters of the installation, tension of loading U and capacity C , as well as maximal work tension of the batherry U_{\max} .

Key words: electrical, energy, vapacitor, tension, capacity, electrohydraulic, effect.

1. INTRODUCTION

It is know the fact that the electrohydraulic effect to generate to the sudden perforation of the electrolyte between of the electrods from the electrohydraulic chamber, under electrical high tension, with which is loaded yhe capacitor batherry, to the sudden discharge of the electrical loaded energy in the capacitor energy. To the sudden discharge energy, to generate a pression impuls which can be utilize in technological purposes.

2. CONDITIONS FOR THE REALIZATION ELECTROHYDRAULIC EFFECT

For the realization electrohydraulic underwater through scintillas discharge is necessary the electrical perforation between electrodes. There are following situations respecting electrical perforation of the interval from the two electrodes and namely >

- If the intensity of the electrical field between electrods $E \geq 360 \text{ KV/m}$ to realise sudden perforation, which is favourable for execution of the technological operations, because in

this case to generate the pression impulse;

- If the intensity of the electrical field betwe enelectrods $30 \text{ KV/m} < E < 360 \text{ KV/m}$ to realise thermal perforation, with heating and place ionization of the liquide with to realise the pression impulse; Clearly, that this situation can not utilise in teghnological purpose;
- If the intensity of the electrical field between electrods $E \leq 30 \text{ KV/m}$ the perforation of the liquide is not possible.

In other papers, to recommend that for the determination of the maximum distance between electrods which produce sudden discharge, to utilise the equation:

$$\delta_{\max E} = 0,06 \cdot \sqrt[3]{C} \cdot U^2 = K_1 \cdot U^2 [\text{mm}] \quad (1)$$

in which:

U - the tension of loading pf the capacitor batherry in KV ;

C - the electrical capacity of the batherry in μF . From the first condition on the electrical field from electrods, result equations (2) and (3):

$$\delta_{\max C} = \frac{U \cdot 1}{360} [m] = \frac{1000}{360} \cdot U [mm] =$$

$$= K_2 \cdot U = 2,777 \cdot U [mm]$$

(2)

$$\delta_{\min} = \frac{U \cdot 1}{30} [m] = \frac{1000}{30} \cdot U [mm] =$$

$$= K_3 \cdot U = 33,333 \cdot U [mm]$$

(3)

where:

$\delta_{\max C}$ - the maximum distance for to realise sudden discharge;

δ_{\min} - the minimum distance for which the perforation of the liquide is not possible.

The angles of inclination pf the rights, in comparisons wirh abscissa axis, are:

- For $\delta_{\max C}$:

$$\alpha = \arctg K_2 = \arctg 2,777 = 70,20^{\circ}$$

(4)

- For δ_{\min} :

$$\beta = \arctg K_3 = \arctg 33,333 = 88,25^{\circ}$$

(5)

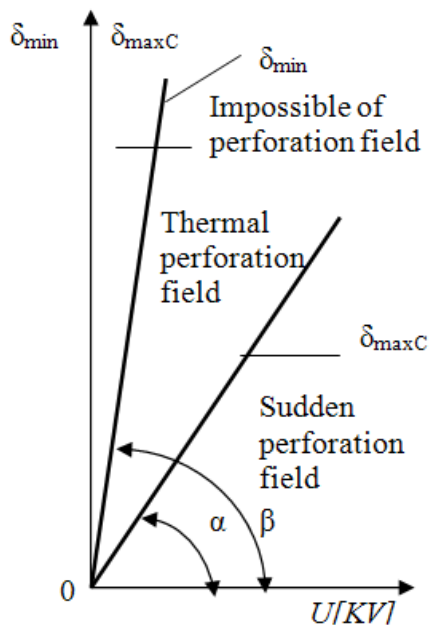


Figure1. The fields for different ways of perforation of the liquide function of the tension and the distance between electrodes.

From the equality equation (1) and (2) result:

$$K_2 \cdot U = 0,06 \cdot \sqrt[3]{C} \cdot U^2 = K_1 \cdot U^2$$

(6)

$$U_e = \frac{K_2}{K_1}$$

(7)

where U_e is tension for which:

$$\delta_{\max C} = \delta_{\max E}$$

(8)

The value $K_2 = 2,777$ and the value

K_1 for the capacity of the instalation from laboratoy $C = 70 \mu F$ is:

$$K_1 = 0,06 \cdot \sqrt[3]{70} = 0,247$$

(9)

For this case result:

$$U_e = \frac{K_2}{K_1} = \frac{2,777}{0,247} = 11,2KV \quad (10)$$

The maximum distance between electrodes in this case is:

$$\delta_{\max e} = K_2 \cdot U = 2,777 \cdot 11,24 = 31,2mm$$

(11)

In figure 3 are represented the two curves:

$$\delta_{\max C} = K_2 \cdot U = 2,777 \cdot U [mm] \quad (12)$$

$$\delta_{\max E} = K_1 \cdot U^2 = 0,247 \cdot U^2 [mm] \quad (13)$$

To find that for $U < U_e$, the condition (15) is principal because if this is accomplished, result that and the the condition (14) is accomplished.

For $U > U_e$ the condition (14) is principal, because if this is accomplished, result that and the the condition (15) is accomplished.

If the capacity of the bathery increase, then the value of the tension U_e decrease. For example, if $C = 350 \mu F$, the value

$$K_1 = 0,06 \cdot \sqrt[3]{350} = 0,422 \quad \text{and}$$

$$U_{e1} = \frac{2,777}{0,422} = 6,6KV$$

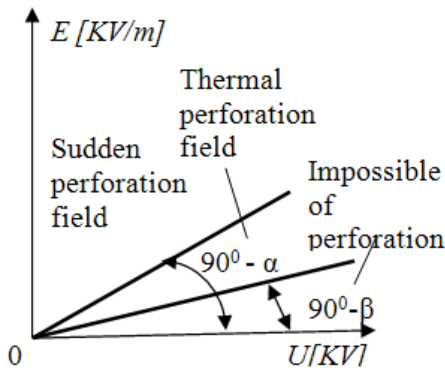


Figure 2. The fields for different ways of perforation of the liquide function of the tension and the intensity of the electrical field

So, with the increase of capacity, decrease the interval for which the condition (15) is principal. For the capacities very large, the maximum distance between electrodes, is determined of the condition (14).

The optimal distance is:

$$\delta_o \approx \frac{\delta_{max}}{2} \tag{14}$$

because the variation of the electrical current in the interval $[0, \delta_{max}]$ is about that in figure 4.

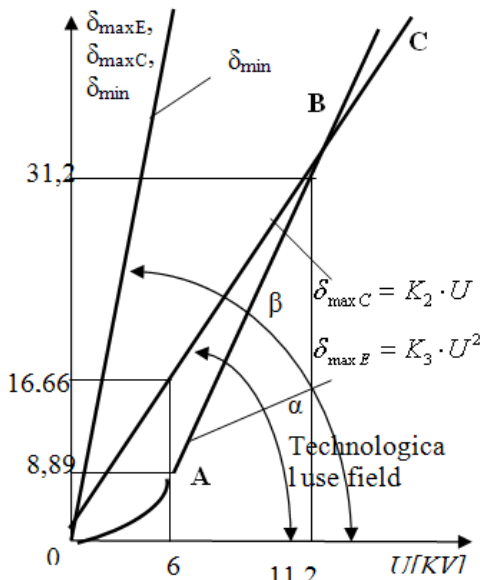


Figure 3. The variation maximum distance between electrodes for the two case δ_{maxC} and δ_{maxE} function of loading tension of the batherry.

The value $\delta_{max} = \delta_{max E}$, if maximum work tension of the insyalation $U_{max} \langle U_e$ and $\delta_{max} = \delta_{max C}$ if maximum work tension of the insyalation $U_{max} \rangle U_e$

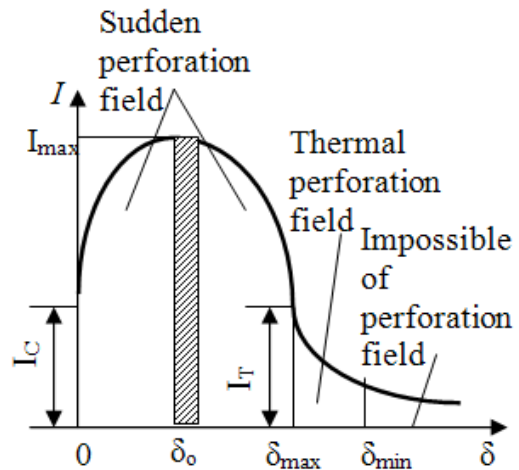


Figure 4. The variation pf the discharge current function of the distance between electrodes.

I_C - the intensity of the current determined in very large part of electronic conducted current: ;

I_T - the intensity of the current determined in very large part of thermal ionization.:

For the capacity of the instalation from laboratory $C = 70 \mu F$, the tension $U_e = 11,2KV$ and maximum work tension $U_{max} = 6KV \langle U_e = 11,2KV$. So, in this case $\delta_{max} = \delta_R = 8,892mm = 8,9mm$. The optimaum value result:

$$\delta_o = \frac{\delta_{max E}}{2} = \frac{8,892}{2} = 4.446mm \approx 4.45mm \tag{15}$$

vvalue with wich have work for texperimentation.

The experimental determinations confirm full previous assumptions.

The technological work comain is under curve OABC from the figure 3.

For the tensions $U_{max} \leq 6KV$, proper for the instalation from plastic deformation

laboratory of the mechanical engineering faculty, maximum and the optimal values to

present in the table

Tabel 1.

Tension U , KV	1	2	3	4	5	6
Maximum distance $\delta_{\max E}$, mm $\delta_{\max E} = K_2 \cdot U^2 = 0,247 \cdot U^2$	0,247	0,988	2,223	3,952	6,175	8,892
Optimal distance δ_0 , mm $\delta_0 = \frac{\delta_{\max E}}{2}$	0,123 \approx 0,1	0,494 \approx 0,5	1,111 \approx 1,1	1,976 \approx 2,0	3,087 \approx 3,1	4,446 \approx 4,5

3. CONCLUSIONS

Virtually, for the determination of the maximum and optimum distance from electrodes, to underwater scintillas discharge, to propose following methpdology:

- Function of the capacity of the capacitor bathery, to determine the value K_2
- To determine the balue of the yension U_e for which the two distances is rqual:

$$U_e = \frac{K_2}{K_1} [KV] \quad (16)$$

- To compare the maximum work tension of the installation U_{\max} with the value U_e
- If $U_{\max} < U_e$ the maximum distance between electrodes is $\delta_{\max E}$;
- If $U_{\max} > U_e$ the maximum distance between electrodes is $\delta_{\max C}$;
- The optimal distance from electrodes id:

$$\delta_o = \frac{\delta_{\max}}{2} \quad (17)$$

The value δ_{\max} from the equation (19) is equal with $\delta_{\max E}$, or with $\delta_{\max C}$,function of

report $\frac{U_{\max}}{U_e}$. Clear, that for $U_{\max} = U_e$, is

whatever which from the two equation to utilise, because to obtain same result.

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